

exceeds the air flow out of the chamber 30 through the leak hole. When the air flow into the chamber 30 is reduced to a certain amount or discontinued (as when the MEMS device 16 is closed) the Braille dot 20, because of its resilient nature, will contract, as described above, and forces the air out of the chamber 30 through the leak hole. The actuator 28 can be operated electrostatically, thermally, piezoelectrically or using shapememory alloys.

[0049] Referring now to FIG. 7A and 7B there are shown detail views of a Braille dot with a MEMS device 16 extended and retracted, respectively. The actuator 28 is a sliding element operating between two electrodes (electrostatic), 281a and 281b depending on to which electrode voltage is applied. In FIG. 7A voltage is being applied to electrode 281b and the slide element 28 is attracted to it, opening a passage to plenum 32 and closing the passage to the vent path 33. In this position air flows into the chamber 30 and the chamber 30 is allowed to pressurize and expand the Braille dot 20. In this the Braille dot 20 is formed by distorting the top surface 46 attached to the frame 24 (which may be part of the housing 22 module 18 and is not shown in FIG. 7A or 7B). The Braille dot 20, is just a dimple in the top surface 46. Referring now to FIG. 7B, voltage is applied to electrode 281a and the slide element 28 is attracted to it closing the passage to the plenum 32 and opening the passage to the vent path 33 and allowing the pressure to vent out of the chamber 30. Without the pressure, the Braille dot 20 contracts, flattening out the Braille dot in the top surface 46. The voltage to the electrodes 281a, 281b is controlled by either the microcontroller 40 through lines 44 or the module microcontroller 45 through lines 44 allowing independent extension and retraction of the Braille dots 20.

[0050] FIG. 8 is a design for a microelectromechanical device that indirectly actuates a Braille dot by opening and closing a valve that allows gas, e.g. air, etc or fluid to exert pressure on a resilient, flexible polymer to form the Braille dot 20. In FIGS. 8A and 8B are shown detail views of a Braille dot 20 with a MEMS device 16 extended and retracted, respectively. The actuators are a pair of MEMS microvalves 284a, 284b which open or close. The MEMS microvalves 284a, 284b can be actuated electrostatically, thermally, piezoelectrically or using thin film shape-memory alloys. In FIG. 8A, the MEMS microvalve 284a is open allowing pressurized gas from the plenum 32 into the chamber 30, while the MEMS microvalve 284b is closed blocking the pressurized gas from leaving the chamber 30. The pressurized gas in the chamber 30 expands the Braille dot 20. In this the Braille dot 20 is formed by distorting the surface covering 45 attached to the frame 24 (which may be part of the housing 22 or module 18 and is not shown in FIG. 8A or 8B). The Braille dot 20, is just a dimple in the top surface 46. Referring now to FIG. 8B, the MEMS microvalve 284a is now closed blocking the flow of pressurized air from the plenum 32 and the MEMS microvalve 284b is now opened allowing the air to evacuate from the chamber 30 to the vent 33. With the pressure vented, the Braille dot 20 contracts, flattening out the dimple on the top surface 46. The voltage to the two the MEMS microvalves 284a, 284b are controlled either directly by the microcontroller 40 or by the module microcontroller 45 to extend and retract Braille dots 20 independent of other Braille dots 20.

[0051] FIGS. 9 and 10 show directly actuated devices using shape memory alloy or piezoelectric based devices.

FIG. 9 is a design for a microelectromechanical device that directly actuates a Braille dot using a thin film shape memory alloy or piezoelectric element to form the Braille dot 20. In FIGS. 9A and 9B, there is shown a detailed view of a Braille dot 24) and MEMS device 16 which uses either a thin film shape memory alloy or piezoelectric element 282 as the actuator. A thin film SMA based microelectromechanical actuator is significantly different than traditional bulk shape memory alloy actuators in size, fabrication techniques, and operation. The mechanical properties of a thin film SMA can be precisely tailored by changing the alloy ratios during fabrication while a macro sized bulk SMA actuator may have regions where the alloy ratio changes within the bulk material of the actuator, these regions will increase power consumption, reduce fatigue resistance and limit life. Thin film SMA actuators have greater fatigue life and improved phase transition characteristics than traditional bulk SMA actuators. The thin film SMA also has faster response and lower power consumption than traditional bulk SMA actuators due to their reduced volume and large surface area which allows the actuator to change from one phase state to another faster than the larger bulk SMA actuators. The rapid response of the thin-film SMA actuators allows a user to quickly scroll through a document without having the refreshable Braille display lag behind. The lower power consumption of a thin film SMA actuator reduces the amount of heat that needs to be dissipated from the actuators during operation and can permit battery operation for use with portable electronic devices. Shape Memory Alloys (SMA's) are a unique class of alloys which have the ability to form two different crystalline phases, defined as martensite and austenite, in response to temperature and strain. SMA's are produced by equiatomically combining at least two component metals into a desired shape, which is then annealed. When produced, the SMA is in the austenite phase, having a certain shape and characterized by low ductility, high Young's modulus and high yield stress. Upon cooling the SMA changes to the martensite phase characterized by high ductility, a low Young's modulus and low yield stress. In the martensite phase, the SMA is easily deformed and can take on a different shape from its austenite or original shape by applying an external strain. The SMA will retain this different shape until it is heated to its austenitic transformation temperature. When the SMA is heated to its austenitic transformation temperature the SMA transitions to its austenite phase and transforms back to its original shape. Similarly, piezoelectric elements 282 can be tailored for the application. FIGS. 9A and 9B also show the application of a direct actuation of the Braille dot 20 without the need of a pneumatic or hydraulic force.

[0052] If a thin film SMA element 282 is used then in FIG. 9A the thin film SMA element 282 is in its martensite phase with the Braille dot 20 retracted. Since the martensite phase is characterized by high ductility, low Young's modulus and low yield stress, the thin film SMA element 282 is easily deformed by external stresses like biasing means 283, shown as a spring in FIG. 10. When heated to its austenitic transfer temperature, the thin film SMA element 282 transitions from its martensite phase to its austenite phase transforming to its austenitic or original shape. The force produced by the biasing means 283 is less than the force produced by the thin film SMA element 282 during this transformation. The thin film SMA element 282, thereby,